

Powder bed fusion processes







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Powder bed fusion processes

- AM process in which thermal energy selectively fuses regions of a powder bed
- First commercial example: Selective laser sintering (SLS), invented by Carl Deckard during his PhD in Texas University in 1987
- Basic set of characteristics:
 - one or more thermal sources
 - methods for controlling powder fusion
 - mechanism for adding and smoothing powder layers
- Laser is the most common thermal source (laser sintering)
 - polymer laser sintering (pLS)
 - metal laser sintering (mLS)

+ Laser Sintering

Baseline description



Figure 20.7 Schematic illustration of the selective-laser-sintering process. *Source*: After C. Deckard and P. F. McClure. Manufacturing, Engineering & Technology, Fifth Edition, by Serope Kalpakjian and Steven R. Schmid. ISBN 0-13-148965-8. © 2006 Pearson Education, Inc., Upper Saddle River, NJ. All rights reserved.

+ Laser Sintering

Baseline description



https://www.youtube.com/watch?v=bgQvqVq-SQU

+ SLS samples





+ Laser Sintering

- The fabrication chamber is maintained at a temperature just below the melting point of the powder
- Heat from the laser need only elevate the temperature slightly to cause sintering. This greatly speeds up the process;
- No supports are required with this method since overhangs and undercuts are supported by the solid powder bed;
- Surface finishes and accuracy are not quite as good as with stereolithography, but material properties can be quite close to those of the intrinsic materials

+ Materials

- Polymers and composites
 - amorphous vs (semi-)crystalline polymers
 - nylon (polyamide), ABS, PVC, and polystyrene, PCL, PLA
 - nylon/polycarbonate powders are health hazards (dangerous to breathe).
 - glass-filled or with other fillers
 - metals encapsulated in plastic.
- Metals
 - low melting metal alloys of nickel bronze, steel, titanium, alloy mixtures, and composites
- Ceramics and ceramic composites
 - Green sand (for sand casting), hydroxyapatite
 - Metal ceramic composites (chemically induced sintering processes)

+ Powder fusion mechanism



* Solid state sintering process





Solid state sintering process

- bonding of the metal, ceramic or plastic powders together when heated to temperatures in excess of approximately half the absolute melting temperature.
- In the industry, sintering is mainly used for metal and ceramic parts (Powder Metallurgy).
- After pressing (compaction) of the powder inside mold for deforming into high densities, while providing the shape and dimensional control, the compacted parts are then sintered for achieving bonding of the powders metallurgically.

Solid state sintering process

- Mechanism: diffusion between powder particles (intrinsically slow)
- Driving force: minimization of the total free energy $E_s = \gamma \times S$ (S=surface)
- Larger the surface to volume ratio, greater is the driving force (smaller particles sinter more rapidly)
- Diffusion rates depends on temperature with an Arrhenius law.

Solid state sintering process in AM

- Sintering process used in additive manufacturing (AM) differs from the Powder Metallurgy, such as:
 - Local sintering, not overall sintering
 - Very short sintering period
 - not use of isostatic pressure
- Laser (heat source) is exposed to sections to be sintered for a very short time. Hard to achieve an ideal sintering.
- In some applications, for achieving the ideal sintering, the finished parts are heated in a separate sintering oven.
- Practically, the solid state sintering is not used as primary fusion mechanism in AM

Solid state sintering process in AM

- Side effects:
 - increase of average particle size of recycled powder
 - "part growth": the final model results bigger due to solid state sintering of new powder at the shell of the model
 - compensation at building scanning strategy
 - removal during post processing
 - decrease of porosity

+ Chemically induced sintering

- It involves the use of thermally activated chemical reactions between
 - two types of powders or
 - powders and atmospheric gases
 to form a by-product which binds the powders
 together
- Primarly used for ceramic materials
 - SiC and O_2 to form composite SiC Si O_2
 - Al and N_2 to form a link between Al and AlN particles
- Limited use in commercial application

Liquid phase sintering and partial melting

- Fusion of powder particles when a portion of constituentes within a collection of powder particles become molten, while other portions remain solid
- Molten constituentes act as "glue"
- Distinction between binder and structural materials
 - separate particles
 - composite particles
 - coated particles
 - no distiction (partial melting)

+ Liquid phase sintering

Separate particles

- Binder material is usually smaller in particle size than the structural material
 - Efficiency in packing
 - Less shrinkage
 - Lower porosity
- Polymeric binder with structural metal particles
- Usually for production of «green» parts



+ Liquid phase sintering

Composite particles

- Binder and structural materials agglomerated together, but distinct at microscopic level
- For «green» parts with higher density
- e.g. glass filled nylon



+ Liquid phase sintering

- Coated particles
- Better absorption of laser energy, more effective binding, better flow properties
- Less amount of binder is required
- Usually with a round shape



Partial melting

Indistinct binder and structural materials

- Very similar to liquid-phase sintering
- Important for noneutectic alloy compositions
- Firstly used in the Direct metal laser sintering (DMLS) machine by EOS



Full melting

- Sintering mechanism most commonly associated with PBF processing for metal alloys and semicrystalline polymers
- Well-bonded, high density structures
 - Nylon polyamide
 - Ti, Stainless stell, CoCr

PROCESS MODELLING

Relevant physical properties

- Melting temperature
- Fluid Dynamic properties
 - Viscosity
 - Surface tension
- Heat conduction properties
 - Thermal conductivity
 - Specific heat
- Thermal expansion

* Melting temperature



+ Viscosity



+ Surface tension



Thermal conductivity and expansion



+ Thermal conductivity



Heat capacity

 c_p (J/kg-K) Material at room T Polymers 1925 Polypropylene Polyethylene 1850 Polystyrene 1170 1050 Teflon increasing $c_{
ho}$ Ceramics Magnesia (MgO) 940 Alumina (Al₂O₃) 775 Glass 840 Metals Aluminum 900 486 Steel Tungsten 138 Gold 128

c_p (specific heat): (J/kg-K) C_p (heat capacity): (J/mol-K)

 Why is c_p significantly larger for polymers?

Selected values from Table 19.1, Callister & Rethwisch 8e.

+ Granulometry and roundness





+ Process parameters

- Laser related parameters
 - laser power, spot size, pulse duration, pulse frequency, etc.
- Scanning relaterd paramters
 - scan speed, scan spacing, and scan pattern
- Powder related parameters
 - particle shape, size and distribution, powder bed density, layer thickness, material properties, etc ...
- Temperature related parameters
 - powder bed temperature, powder feeder temperature, temperature uniformity, etc ...

+ Scanning strategies



- Typical layer thickness are 0.02 to 0.15 mm
- Usually continuous wave laser are used

Applied energy density

- $E_A = P/(U \times SP)$
 - E_A = applied energy density (Andrews number) [J/m²]
 - -P = laser power [W]
 - U = scan velocity [m/s]
 - SP = scan spacing between parallel scan lines [m]

* Applied energy density



Laser Sintering – support strategies

Angled surfaces and holes



The powder in the build chamber does not provide any support to the part as it builds, so any angled surfaces will ideally be self-supporting



If the angle is too acute, the surface will need a supporting structure built in as part of the model. This supporting structure will then need to be removed by machining or wire cutting, increasing energy use



The minimum angles that will be self supporting are approximately: - Stainless steels: 30 degrees - Inconels: 45 degrees - Titanium: 20-30 degrees - Aluminium: 45 degrees - Cobalt Chrome: 30 degrees



If the angle is near the point where it needs supports, the downward facing surface will become rough an may require considerable post-finishing



Small holes can be accomodated easily. Holes of less than 6mm diameter are ideal



Larger circular holes will result in a roughened surface at the top which may need post-machining



Large holes will require support structures to be added in the centre to prevent the part collapsing or becoming distorted during the build process. These supports will need to be removed by wire cutting or machining



If the hole has an angled or arched upper area it will probably not require any supports. This is one of the features of DMLS that can have a significant impact on the design process

Laser Sintering – orientation strategies

Direction of build and cross sections



As the recoater blade passes over the part, depositing another layer of powder, it can touch the layer below, sometimes with some force. The orientation of the part is, therefore, important.

The ideal geometry is a circular profile which provides a smooth lead in for the blade, and a stable cross section as it builds.



An open 'U' or similar shape is also ideal, as the lead in for the blade is again rounded, and the basic profile will be strong as it builds, resisting the force of the recoating blade.



The worst case' geometry would be a thin section parallel to the recoater blade. The blade will tend to 'bounce' off the parallel wall, and the section itself will not resist the force of the blade as it builds.



Any flat surfaces need to be at least 5 degrees from parallel with the blade to allow the blade to touch the part at a point, not a face



In addition to touching the part at an angle, it helps if the geometry is inherantly stiff, which will resist bending forces as the recoater blade passes over the part.



Long, thinner parts with rounded ends will build well, as they also provide a smooth lead in for the blade and are inherantly stiff. However, all these issues need to be considered in parallel with the other limits (build angles, etc) mentioned elsewhere in this section.

Laser Sintering – orientation strategies

Part strength during the build process



As the recoater blade passes over the building part, more force will be applied to the geometry as it gets tailer. As a rule of thumb, the ratio between the section and the height should be approximately 8:1



The exact proprious will always depend on the specific geometry, but if the section gets too high, there is a danger that the recoater blade will bend the part, and possibly damage itself in the process, terminating the build sequence.



To prevent these problems, vertical sections need to be bridged at certain points. The best method of achieving this will be to use 'arches' to avoid the creation of downward facing flat surfaces,



Even a part that will be strong when it is finished may need some support during the build process. This triangular section will be very weak as the build gets close to the apex.



This kind of structure may need a simple support structure up the middle to provide some rigidity before the part is completed.



If the reason for the open structure is simply weight reduction, it may be easier to perforate it with holes (ideally less than 6mm in dia) that will reduce weight, but not require any supports.
POWDER HANDLING

Powder handling systems

- Have a sufficient volume
- Deliver the right quantity of powder (without waste)
- Provide a smooth, thin, repeatable layer of powder
- Limit shear forces on previous layer
- As particle size decreases
 - Interparticle friction and electrostatic forces increases (limit flowability)
 - More reactivity (including explosion)
 - Airborne and clouding optics
 - More difficult to be handled

Powder handling systems

• Hopper



Vibrating blade or roller

Powder recycling

- Fraction based mixture might be
 - 1/3 unused powder,
 - 1/3 overflow/feed powder, and 1/3
 - build platform powder.

Plastic Laser Sintering

• For direct manufacture of styling models, functional prototypes, patterns for plaster, investment and vacuum casting, for end products and spare parts.





- Volvo Steering Wheel
- Engine Block Pattern
- Plaster Invest. Pattern



Metal Laser Sintering

- For direct production of tooling, including for plastic injection molding, metal die casting, sheet metal forming as well as metal parts, directly from steel based and other metal powders.
 - A gear for Volvo Corp.
 - Die Cast Parts (500 Al parts produced)
 - Motor Housing



* Some available metals

| Materiale EOS | R | Rp0,2 | A | test di Fatica (*) | Durezza |
|---------------|-----------|-----------|---------|--------------------|---------|
| | MPa | MPa | % | MPa | HRC |
| AlSi10Mg | 405-445 | 230-275 | 3,5-6,5 | 97 | n.d. |
| In718 | 980-1060 | 634-780 | 27-31 | n.d. | 30 |
| SS PH1 | 1050-1150 | 650-850 | 16-17 | 30-35 | >90 HRB |
| Ti6Al4V | 1200-1230 | 1060-1070 | 10-11 | n.d. | 35-40 |
| CoCr MP1 | 1200-1350 | 800-1060 | 11-24 | 560 | 35-45 |

Fonte: EOS

+ Some available metals

- Grana molto fine e distribuzione omogenea dei componenti stechiometrici
- Rispetto norme ISO e ASTM per la composizione chimica
- Proprietà meccaniche similie e superiori a prodotti equivalenti da barra, fusione e forgiatura a freddo (fonte EOS)
- Le caratteristiche metallurgiche sono migliori della fusione a "cera persa" (Investment casting). Infatti nella microfusione laser selettiva si arriva a fusione completa e risolidificazione in tempi brevissimi (frazioni di secondo) e non si dà tempo al "grano" di accrescere (cosa che avviene nell'investment casting)

+ Some avaliable metals

Micrografia di Stainless Steel GP1 mostra una struttura completamente fusa, densa. *Vista trasversale.*



Fonte: EOS

Micrografia di Stainless Steel GP1 Vista da sopra.



Fonte: EOS







* Some avaliable metals

Micrografie di campioni di CobaltChromeMP1



MP1 produce parti con strutture a grana molto fine e dimensioni tipiche di 0.3-0.6 µm

+ Sand Laser Sintering

- Laser Sintering System for direct, boxless manufacture of sand cores and moulds for metal casting.
 V6-24 Valve Cylinder Head.
 - Impeller
 - Steering Block for a car







+ DTM Sinterstation 2500



| Volume di lavoro | 380 X 330 x 460 mm |
|------------------------------|--------------------|
| Laser | CO ₂ |
| Potenza | 50 / 100 W |
| Spot | 0.42 mm |
| Velocità di scansione | 5000 mm/sec |
| Precisione di posizionamento | 0.05 mm |
| Spessore layer | 0.1 mm |

METU SYSTEM

EOS EOSINT P380 Rapid Prototyping System

| General Properties | |
|-----------------------------------------------------------------|-----|
| Plastic Laser Sintering System X,Y Axes Alternating Scanning | |
| Technical Specifications | |
| Work Envelope: | |
| -X Axis: 340 mm | |
| -Y Axis : 340 mm | 0 - |
| -Z Axis : 600 mm | 4 |
| Layer Forming Thickness: | |
| 0.15mm +/-0.05 mm | |
| Max Laser Power: 50 W | |
| Z Axis Production Speed: 30 mm / saat | |
| Max Scanning Speed: 5 m/s | |

+ Eosint P360



Advantages:

- Cheap and no harmed healthy material,
- Large selection of used materials,
- Is not needed supported construction,
- Decreasing of destruction possibility of inside stresses.

Disadvantages:

- Roughness surface after final modification it means "stairs" effect,
- Porosity of components,
- Different intensity in various parts of generated components,
- Material transformations are needing cleaning of the production device

- Process is wall thickness dependent. (not suitable for massive parts)
- Process involving internal stresses in the parts need additional annealing
- Process requiring strong supports for parts fasten during the manufacturing (not only for heat transfer)
- Need to use build plates of the same material than the powder used in the machine (e.g.: more expensive for titanium powder)
- Cutting tool necessary (eg: a saw) in order to release the parts from the build plate

- Surface finishing technologies
 - Tumbling
 - Blasting
 - Chemical and/or electrochemical polishing
 - Abrasive Flow Machining (AFM)
 - Thermal Energy Method (TEM)
 - Robotic and CNC polishing
 - Laser Polishing / Ablation
 - Electron-beam polishing (EBEST)

+ Future trends

- Increase of working volume with several laser heads
- Automatic recovery of unbounded powder
- Repeatibility of the process

ELECTRON BEAM MELTING

EBM

Electron Beam Melting (EBM)

- Electron Beam Melting (EBM) is a type of rapid prototyping for metal parts. The technology manufactures parts by melting metal powder layer per layer with an electron beam in a high vacuum. Unlike some metal sintering techniques, the parts are fully solid, void-free, and extremely strong.
- EBM is also referred to as Electron Beam Machining.
- High speed electrons .5-.8 times the speed of light are bombarded on the surface of the work material generating enough heat to melt the surface of the part and cause the material to locally vaporize.
- EBM does require a vacuum, meaning that the workpiece is limited in size to the vacuum used. The surface finish on the part is much better than that of other manufacturing processes.
- EBM can be used on metals, non-metals, ceramics, and composites.





+ Electron Beam Melting (EBM)

- Dispensed metal powder in layers
- Cross-section molten in a high vacuum with a focused electron beam
- Process repeated until part is completed
- Stainless steel, Titanium, Tungsten parts
- Ideal for medical implants and injection molds
- Still very expensive process



+ Examples of EBM

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ARCAM A2 machine for direct metal deposition





Components made of Ti and Co-Cr alloys





Biomedical components made of Ti alloys

+ EMB benefit

- High productivity
- Suitable for very massive parts
- No residual internal stress (constant 680-720°C build temperature)
- Less supports are needed for manufacturing of parts
- Possibility to stack parts on top of each other (mass production)
- Sintered powder = good for thermal conductivity = less supports
- Process under vacuum (no gaz contaminations)
- Very fine microstructures (Ti6Al4V), very good mechanical and fatigue results (Ti6Al4V)

+ EBM drawbacks

- Powder is sintered -> tricky to remove (e.g. interior channels)
- Long dead time between 2 productions (8 hours for cooling – A2, A2X, A2XX systems)
- Tricky to work with fine powder
- Expensive maintenance contract

 Electron Beam Melting (EBM)



- Metallic powder deposited in a powder bed
- Electron Beam
- Vacuum
- Build temperature: 680-720°C

 Laser Beam Melting (LBM)



- Metallic powder deposited in a powder bed
- Laser Beam
- Argon flow along Ox direction
- Build temperature: 200°C

| Characteristic | Electron beam melting | Metal laser sintering | |
|----------------------|--------------------------------|-----------------------------------|--|
| Thermal source | Electron beam | Laser | |
| Atmosphere | Vacuum | Inert gas | |
| Scanning | Deflection coils | Galvanometers | |
| Energy absorption | Conductivity-limited | Absorptivity-limited | |
| Powder preheating | Use electron beam | Use infrared or resistive heaters | |
| Scan speeds | Very fast, magnetically driven | Limited by galvanometer inertia | |
| Energy costs | Moderate | High | |
| Surface finish | Moderate to poor | Excellent to moderate | |
| Feature resolution | Moderate | Excellent | |
| Materials | Metals (conductors) | Polymers, metals and ceramics | |
| Powder particle size | Medium | Fine | |

| | LBM | EBM | |
|---------------------------------|-------------------------------------------------------|-----------------------------------------------|--|
| Size (mm) | 250 x 250 x 350*1 | 210 x 210 x 350* ² | |
| Layer thickness (µm) | 30 - 60 | 50 | |
| Min wall thickness (mm) | 0.2 | 0.6 | |
| Accuracy (mm) | +/- 0.1 | +/- 0.3 | |
| Build rate (cm ³ /h) | 5 – 20 | 80 | |
| Surface roughness (µm) | 5 – 15 | 20 - 30 | |
| Geometry limitations | Supports needed everywhere (thermal, anchorage) | Less supports but powder is sintered | |
| Materials | Stainless steel, tool steel, titanium, aluminum, | Only conductive materials (Ti6Al4V, CrCo,) | |
| | | *1 SLM Solutions 250HL | |

| | | | EOS | SLM | Concept Laser | Renishaw | ARCAM |
|------------|----------------------|--------|-----------------------------|-----------------------------|------------------|-----------------------------|-----------------------------|
| | | | M270 | 250HL | M1 | AM250 | A1 |
| Ga | s di processo | | Argon o Azoto | Argon o Azoto | Argon o Azoto | Argon o Azoto | |
| cor | isumo di gas | Lt/h | | 90 | 1000 | 5-30 | |
| Pot | enza del laser | W | 200 - 400 | 200 - 400 | 200 - 400 | 200 - 400 | 50-3000 |
| Ma: | < dimensione | mm | $250 \times 250 \times 215$ | $248 \times 248 \times 250$ | 250 ×250 ×250 | $245 \times 245 \times 300$ | $200 \times 200 \times 180$ |
| Са | pacità produttiva | cmc/h | 2 - 20 | 20 | 2 - 20 | 5 - 20 | 55-80 |
| Vel | ocità scansione lase | m/s | | 20 | 7 | 2 | 8000 |
| Spe | essore layers | micron | 20-60 | 20 - 75 | 20-80 | 20 - 100 | |
| For | mato file | | STL | STL | STL | STL | STL |
| Pre | cisione | mm | +/- 0,05 | | +/- 0,05 | | +/- 0,20 |
| Ru | gosità | micron | 4-6 | 4-6 | 4-6 | 4-6 | 25-35 |
| | | | | 1.4404 (316L) | | | |
| | Acciaio inox | | 17-4 PH1 | 1.4542 (17-4 PH) | 1.4404 | 1.4404 | |
| ali | 0i-i | | Managian | 4 0044 (1140) | 4 0700 | 1 00 4 4 | |
| ter | Acciaio per stampi | | Maraging | 1.2344 (H13) | 1.2709 | 1.2344 | |
| Ma | | | | | CoCr (F75), CrCo | | |
| ali | Superlega CoCr | | CoCr ASTMF75 | CoCr ASTMF 75 | (dentale) | CoCr ASTMF75 | CoCrMo ASTM F75 |
| <u>Cip</u> | | | | Ti6Al4V, Ti6Al7Nb, | | Ti-6Al-4V e Ti-6Al- | |
| i,⊟ In | Titanio | | Ti6A4V | Titanio puro | Titanium Grade 5 | 7Nb | Ti6Al4V |
| | | | | | | | |
| | Leghe di Nickel | | Inconel 625, 718 | Inconel 625, 718 | Inconel 625 | inconel 718 e 625 | |
| | Alluminio | | AlSi10Mg | AlSi12 | AlSi10Mg, AlSi12 | AlSi12 | |





+ PBF process variant



MULTIJET FUSION

* Multijet Fusion

- https://www.youtube.com/watch?time_continue=1&v=VXntl3ff5tc
- https://www.youtube.com/watch?v=qEPqlVs11KM



+ Multijet Fusion



Fused

+ Multijet Fusion




+ Multijet Fusion





+ MultiJet Fusion - Materials

HP 3D printing materials provide optimal output quality and high reusability at a low cost per part. Engineered for HP Multi Jet Fusion technology, these materials test the limits of functional part creation, optimizing cost and part quality, while also delivering high¹⁰ and, in many cases, industry-leading reusability⁸ at the lowest cost per part.²

HP 3D High Reusability PA 12

HP 3D High Reusability PA 12 produces strong, functional, detailed complex parts and helps reduce total cost of ownership.¹¹ This robust thermoplastic is ideally suited for complex assemblies, housings, enclosures, and watertight applications. It provides the best balance between mechanical properties and reusability,¹² and provides biocompatibility certifications.¹³ It also delivers consistent performance—while achieving 80% surplus powder reusability⁸ at the lowest cost per part.²

HP 3D High Reusability PA 12 Glass Beads

Ideal for applications requiring high stiffness like enclosures and housings, fixtures and tooling, HP 3D High Reusability PA 12 Glass Beads is a 40% glass bead filled thermoplastic material with both optimal mechanical properties and high reusability.¹⁰ It provides dimensional stability along with repeatability.¹⁴ Customers experience quality results at a low cost per part and get consistent performance while achieving 70% surplus powder reusability.¹⁵

HP 3D High Reusability PA 11

HP 3D High Reusability PA 11 is designed for the production of strong, ductile,¹⁶ functional parts including prostheses, insoles, sports goods, snap fits, living hinges, and more. Providing the lowest cost per part,² HP 3D High Reusability PA 11 is a cost-efficient material offering industryleading surplus powder reusability,⁸ and is made from renewable sources.¹⁷ It offers excellent chemical resistance¹⁸ and enhanced elongation-at-break.¹⁶

Thermoplastics + glass beads

+ MultiJet Fusion

HP Jet Fusion 3D 4210/4200/3200 Printer

| Printer performance | Technology | HP Multi Jet Fusion technology |
|---------------------------|---------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------|
| | Effective building volume | 380 x 284 x 380 mm (15 x 11.2 x 15 in) |
| | Building speed | 3200 Printer: 2800 cm ³ /hr (170 in ³ /hr) ²¹ 4210/4200: 4500 cm ³ /hr (274 in ³ /hr) ²² |
| | Layer thickness | 3200 Printer: 0.08 mm (0.003 in) 4210/4200: 0.07 to 0.08 mm (0.0027 to 0.0031 in) |
| | Print resolution (x, y) | 1200 dpi |
| Dimensions (w x d x h) | Printer | 2210 x 1200 x 1448 mm (87 x 47 x 57 in) |
| | Shipping | 2300 x 1325 x 2068 mm (91 x 52 x 81 in) |
| | Operating area | 3700 x 3700 x 2500 mm (146 x 146 x 99 in) |
| Weight | Printer | 750 kg (1653 lb) |
| | Shipping | 945 kg (2083 lb) |

Directed energy deposition methods

LASER ENGINEERED NET SHAPING



• Direct energy deposition



- Fully Dense Metal parts with good metallurgical properties
- Laser melts metal powder
- Powder delivered coaxially with laser
- Inert gas protects weld pool
- Near net shape with some finish machining

- In addition to titanium, a variety of materials can be used such as stainless steel, copper, aluminum etc.
- Materials composition can be changed dynamically and continuously, leading to objects with properties that might be mutually exclusive using classical fabrication methods.
- Has the ability to fabricate fully-dense metal parts with good metallurgical properties at reasonable speeds;
- Objects fabricated are near net shape, but generally will require finish machining.



Before and after finish machining



120x120x120 cm LENS Machine

+ LENS (Other names)

Capability of in situ repair



https://www.youtube.com/watch?v=d2foaRi4nxM

